

Reconstruction of 3-D Dense Cardiac Motion from Tagged MRI Sequences

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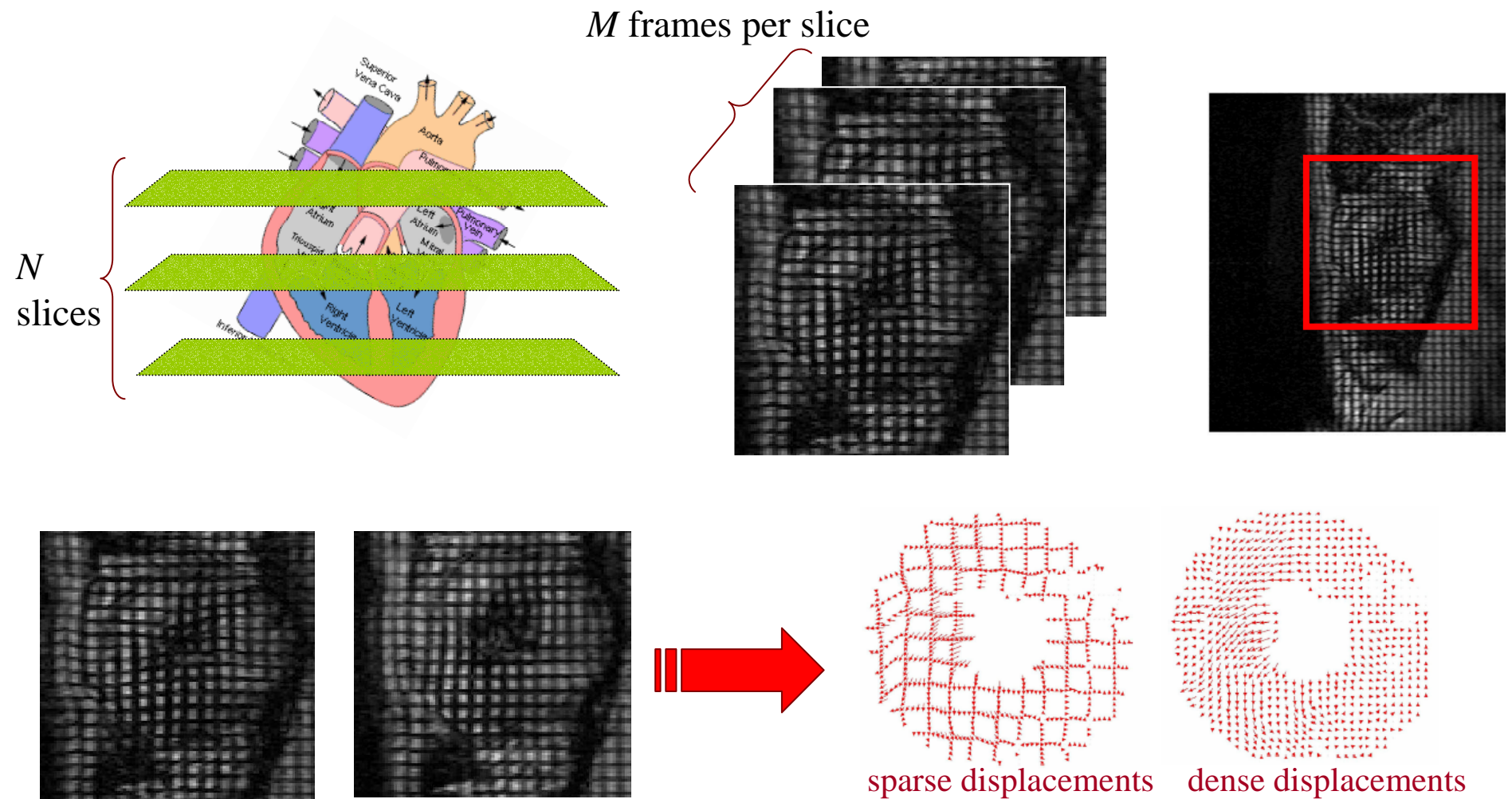
Carnegie Mellon University, Pittsburgh, PA, USA

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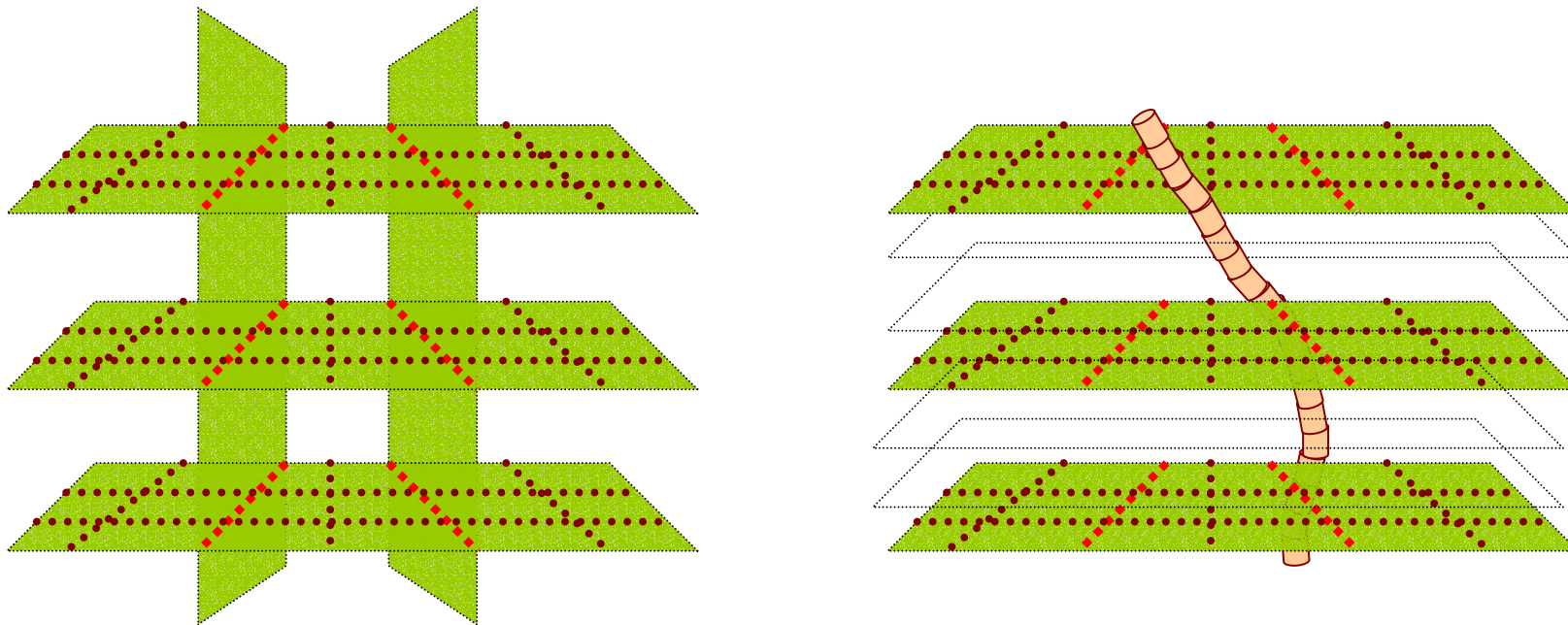
Outline

- **Introduction**
- **Methodology: Prior knowledge + MRI data**
 - Myocardial Fiber Based Structure
 - Continuum Mechanics
 - Constrained Energy Minimization
- **Results and Conclusions**

2-D Cardiac MRI Images

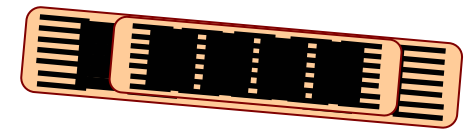
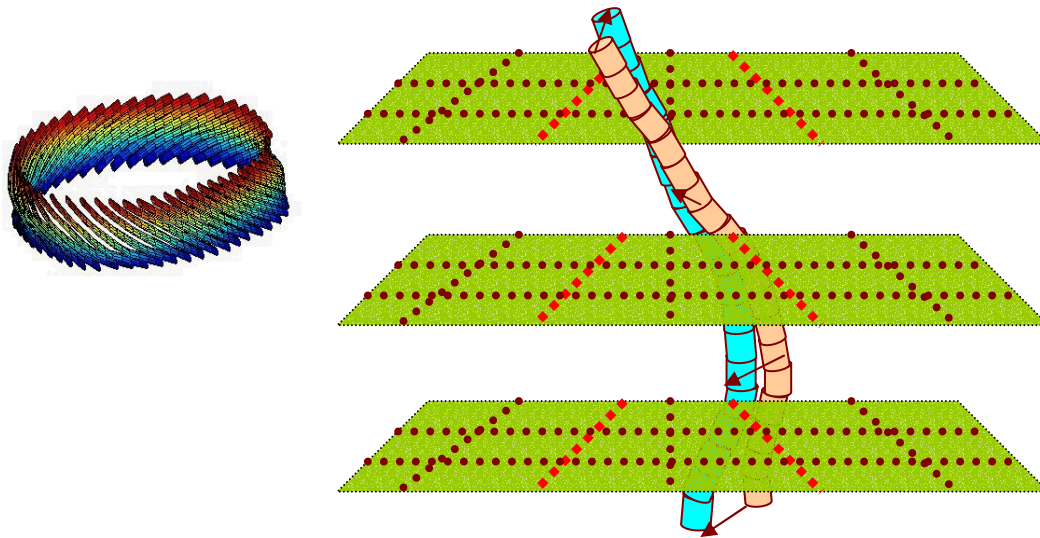


3-D Reconstruction: myocardial fiber model

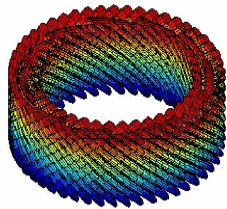


Use a fiber based model to find the correspondence between transversal slices.

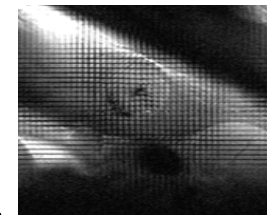
3-D Reconstruction: fiber deformation model



Use continuum mechanics to describe the motion of fibers.



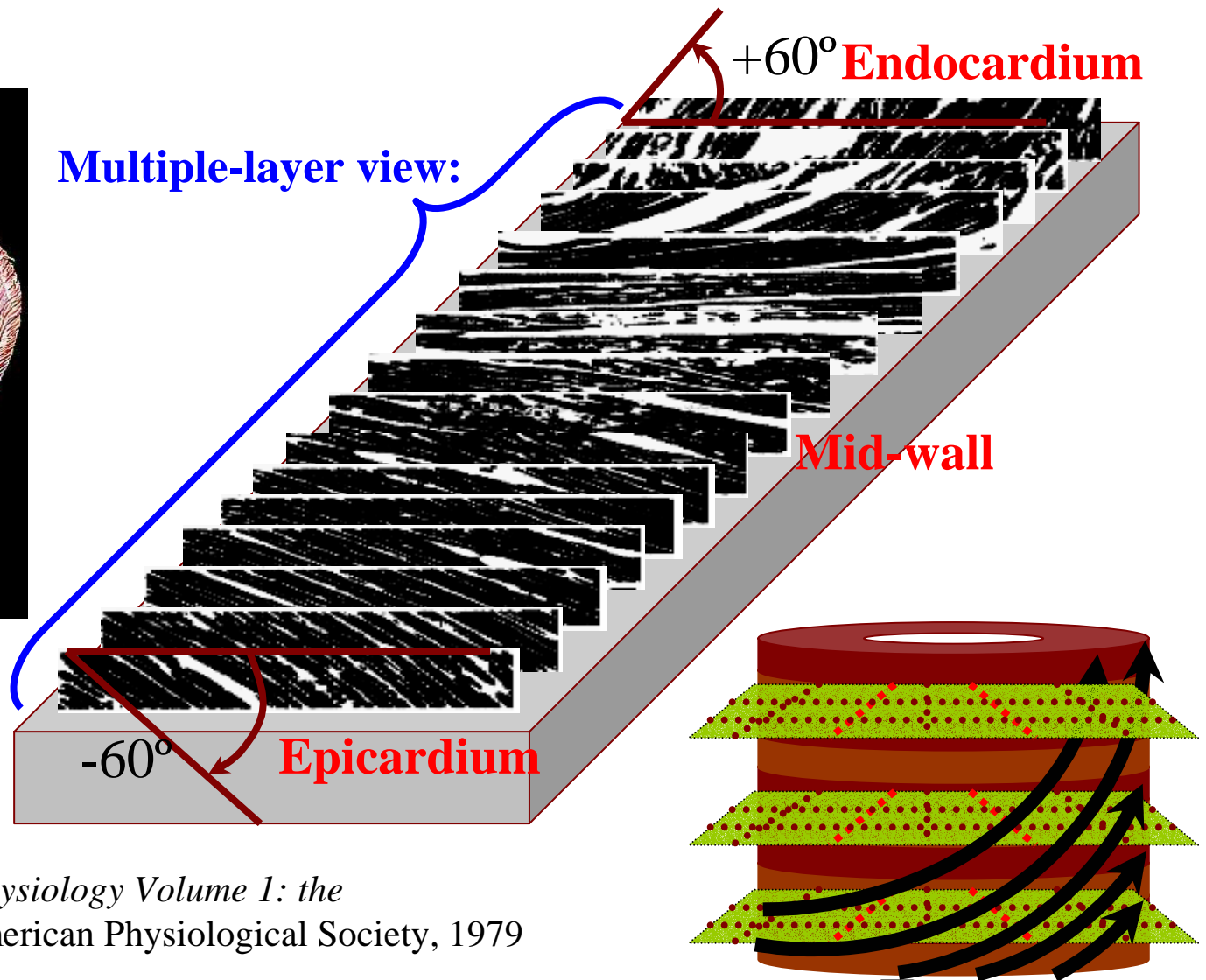
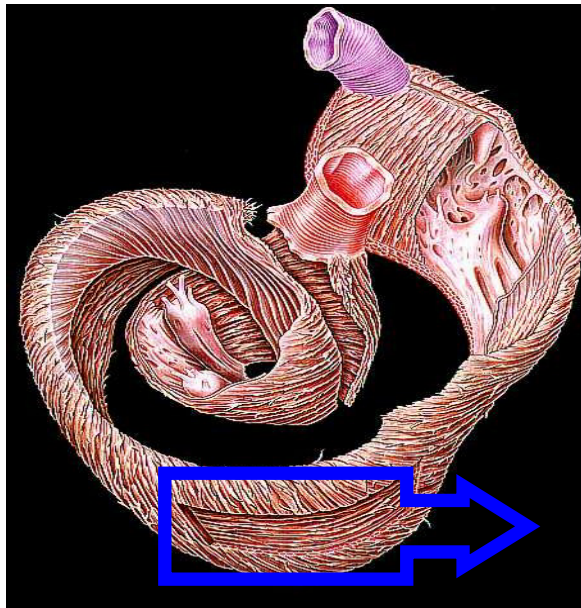
Fit the model to MRI data by
constrained energy minimization



Outline

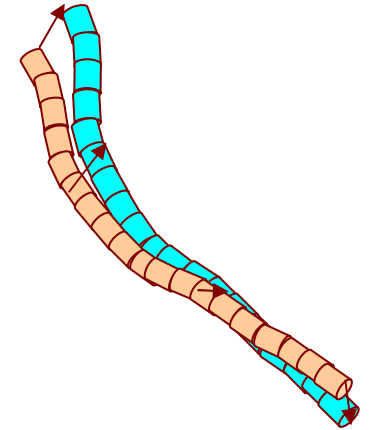
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Prior Knowledge: myocardial anatomy

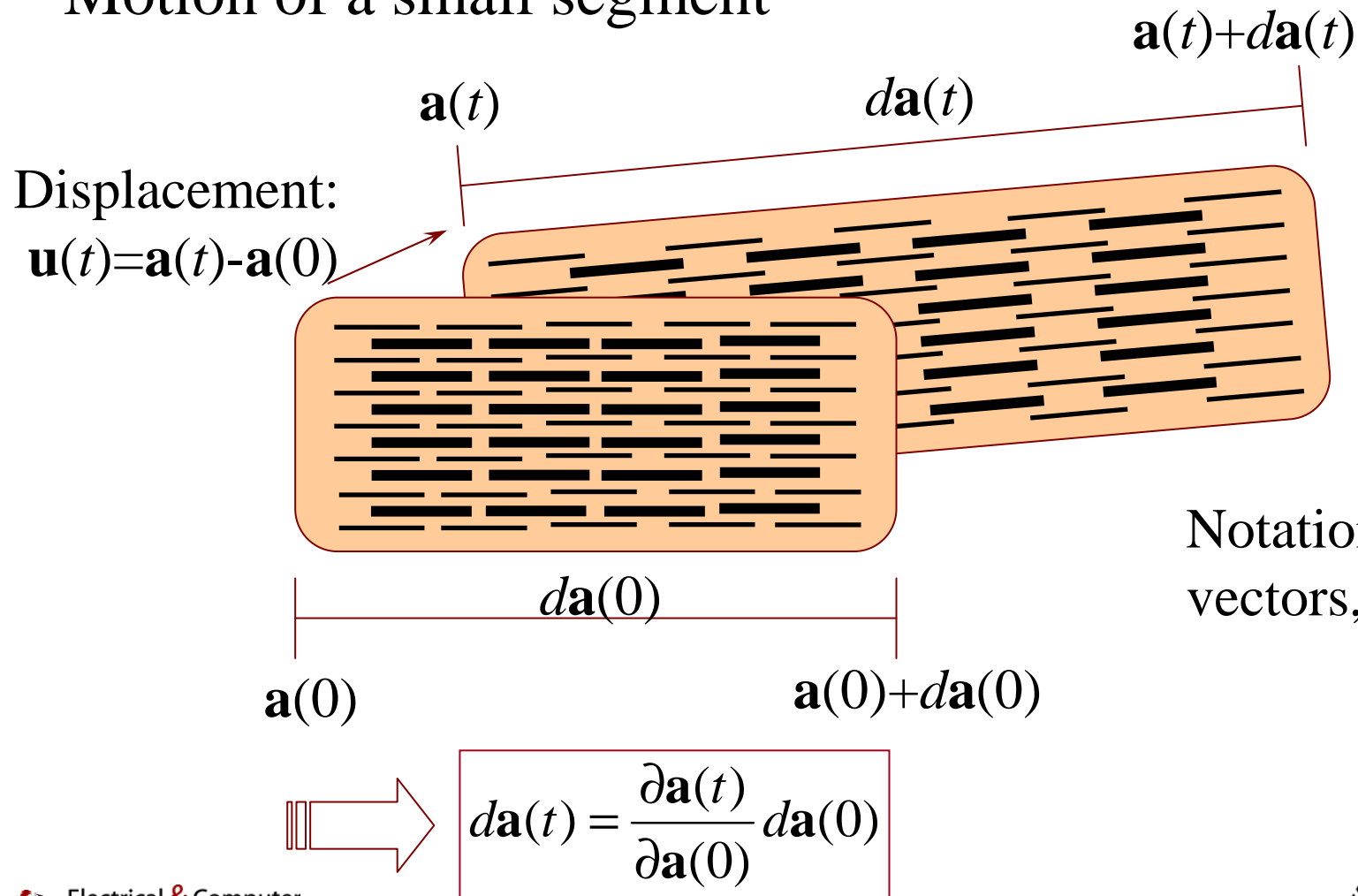


Streeter, in *Handbook of Physiology Volume 1: the Cardiovascular System*, American Physiological Society, 1979

Prior Knowledge: fiber dynamics



Motion of a small segment



Notations are column vectors, ex:

$$\mathbf{a}(t) = \begin{bmatrix} a_1(t) \\ a_2(t) \\ a_3(t) \end{bmatrix}$$

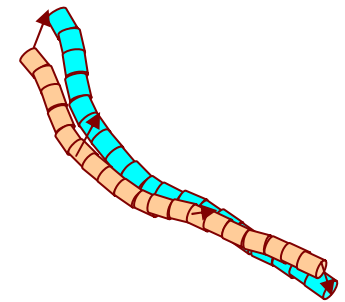
Deformation Gradient Matrix

$$\mathbf{F}(t) = \frac{\partial \mathbf{a}(t)}{\partial \mathbf{a}(0)} = \begin{bmatrix} \frac{\partial a_1(t)}{\partial a_1(0)} & \frac{\partial a_1(t)}{\partial a_2(0)} & \frac{\partial a_1(t)}{\partial a_3(0)} \\ \frac{\partial a_2(t)}{\partial a_1(0)} & \frac{\partial a_2(t)}{\partial a_2(0)} & \frac{\partial a_2(t)}{\partial a_3(0)} \\ \frac{\partial a_3(t)}{\partial a_1(0)} & \frac{\partial a_3(t)}{\partial a_2(0)} & \frac{\partial a_3(t)}{\partial a_3(0)} \end{bmatrix}$$

$$= \mathbf{I} + d\mathbf{F}(t) = \mathbf{I} + \frac{\partial \mathbf{u}(t)}{\partial \mathbf{a}(0)} = \mathbf{I} + \begin{bmatrix} \frac{\partial u_1(t)}{\partial a_1(0)} & \frac{\partial u_1(t)}{\partial a_2(0)} & \frac{\partial u_1(t)}{\partial a_3(0)} \\ \frac{\partial u_2(t)}{\partial a_1(0)} & \frac{\partial u_2(t)}{\partial a_2(0)} & \frac{\partial u_2(t)}{\partial a_3(0)} \\ \frac{\partial u_3(t)}{\partial a_1(0)} & \frac{\partial u_3(t)}{\partial a_2(0)} & \frac{\partial u_3(t)}{\partial a_3(0)} \end{bmatrix}$$

Deformation gradient $\mathbf{F}(t)$ is a function of displacement $\mathbf{u}(t)$.

Strain



- Strain is the **displacement per unit length**, and is written mathematically as $\mathbf{S} = \frac{1}{2}(\mathbf{F}^T \mathbf{F} - \mathbf{I})$

$$\mathbf{S} = \frac{1}{2} [(\mathbf{I} + d\mathbf{F})^T (\mathbf{I} + d\mathbf{F}) - \mathbf{I}] = \frac{1}{2} [d\mathbf{F}^T + d\mathbf{F} + d\mathbf{F}^T d\mathbf{F}]$$

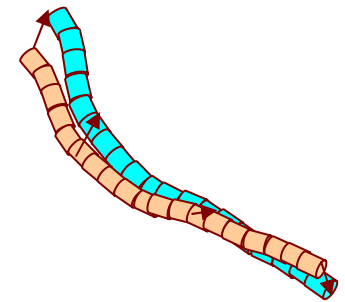
Ref: Y.C. Fung, *A First Course in Continuum Mechanics*, 3rd ed., Prentice-Hall, New Jersey, 1994

- When strain is small, it is approximated as

$$\mathbf{S} \approx \frac{1}{2} [d\mathbf{F}^T + \mathbf{I} + d\mathbf{F} + \mathbf{I}] - \mathbf{I} = \frac{1}{2} (\mathbf{F}^T + \mathbf{F}) - \mathbf{I}$$

(Note: S is symmetric)

Linear Strain Energy Model



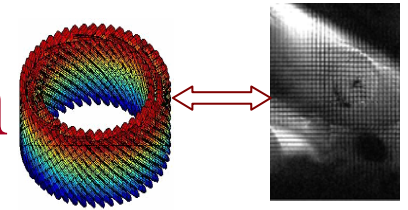
- \mathbf{S} is symmetric, so we vectorize the entries at upper triangle.

$$\mathbf{S} = \begin{bmatrix} S_{11} & S_{12} & S_{13} \\ & S_{22} & S_{23} \\ & & S_{33} \end{bmatrix} \rightarrow \mathbf{s} = [S_{11}, S_{22}, S_{33}, S_{12}, S_{13}, S_{23}]^T$$

- Let \mathbf{C} describe the material properties. It can be shown the linear strain energy is $e = \mathbf{s}^T \mathbf{C} \mathbf{s} = e(\mathbf{u})$
- The entire energy of the heart:

$$E(\mathbf{U}) = \sum_{\forall \text{fibers}} \sum_{\forall \text{segments}} e(\mathbf{u}) = \sum_{\forall \text{fibers}} \sum_{\forall \text{segments}} \mathbf{s}^T \mathbf{C} \mathbf{s}$$

Constrained Energy Minimization



$$E(\mathbf{U}, \lambda) = \gamma_1 E_{int}(\mathbf{U}) + \gamma_2 E_{ext}(\mathbf{U}) + \lambda E_{con}(\mathbf{U})$$

$$E_{int}(\mathbf{U}) = \sum_{\forall \text{fibers}} \sum_{\forall \text{segments}} \mathbf{s}^T \mathbf{C} \mathbf{s}$$

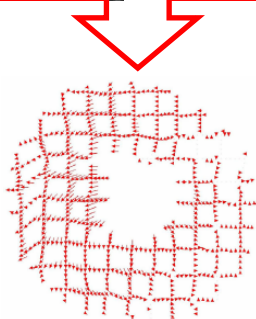
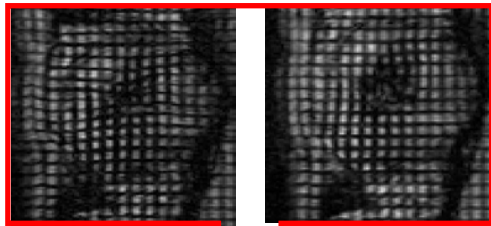
- Internal energy: continuum mechanics governs the fibers to move as smooth as possible.

$$E_{ext}(\mathbf{U}) = \|\mathbf{I}(t) - \mathbf{I}(t+1)\|^2$$

- External energy: pixel intensities of fibers should be kept similar across time.

2-D Displacement Constraints

$$E(\mathbf{U}, \lambda) = \gamma_1 E_{int}(\mathbf{U}) + \gamma_2 E_{ext}(\mathbf{U}) + \lambda E_{con}(\mathbf{U})$$



D: 2-D displacements of the taglines

$\Theta\mathbf{U}$: picks the entries of \mathbf{U} corresponding to **D**

2-D displacement constraints: $\Theta\mathbf{U}=\mathbf{D}$

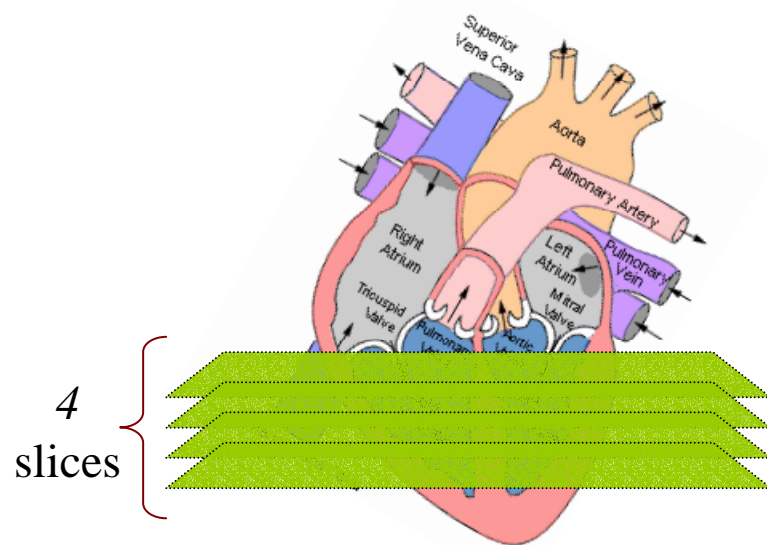
λ : Lagrange multiplier

$$E(\mathbf{U}, \lambda) = \gamma_1 E_{int}(\mathbf{U}) + \gamma_2 E_{ext}(\mathbf{U}) + \lambda \|\Theta\mathbf{U} - \mathbf{D}\|^2$$

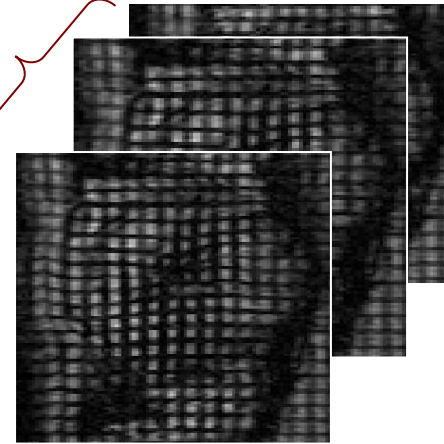
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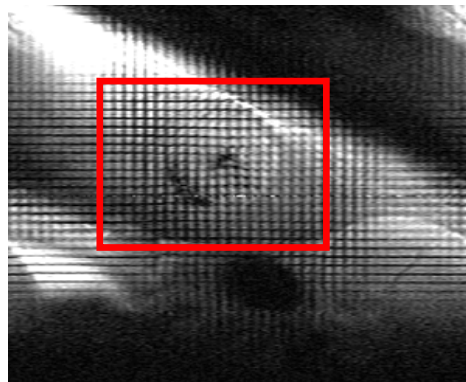
Data Set



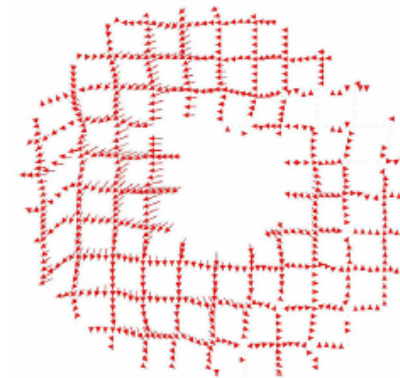
10 frames per slice



256×256 pixels per image

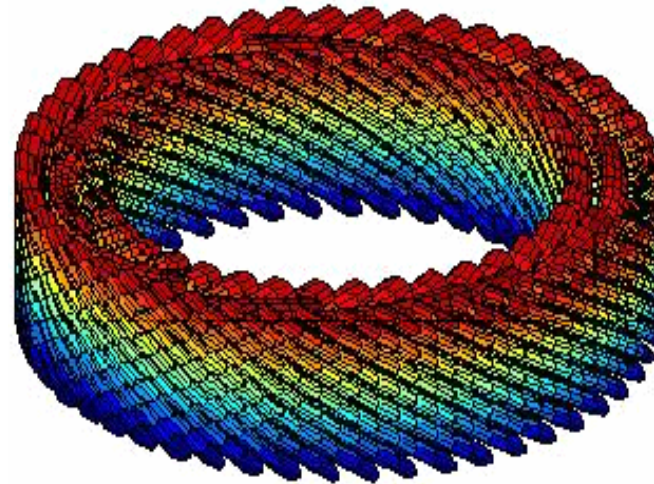
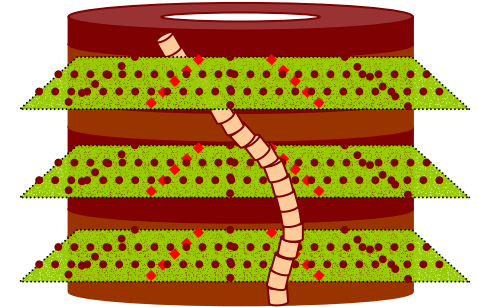


- Transplanted rats with heterotropic working hearts.
- MRI scans performed on a Bruker AVANCE DRX 4.7-T system

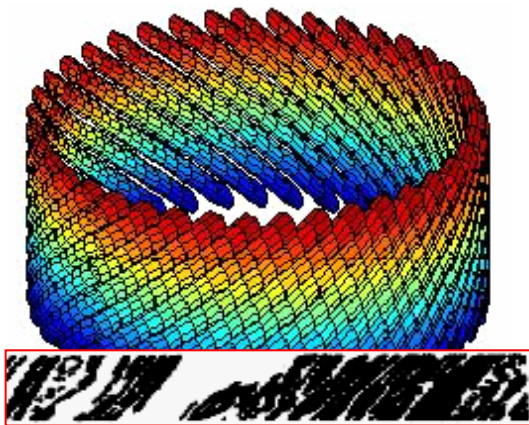


Y. Sun, Y.L. Wu, K. Sato, C. Ho, and J.M.F. Moura, *Proc. Annual Meeting ISMRM 2003*

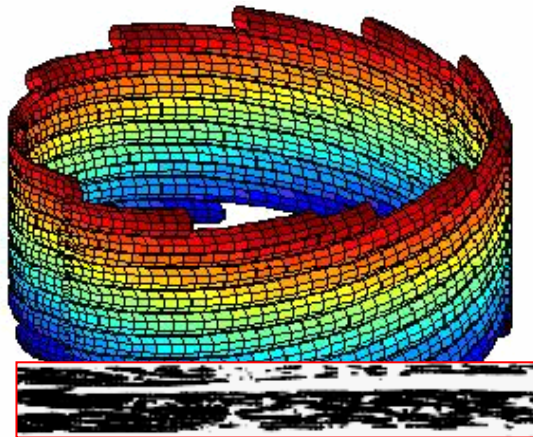
Fiber Based Model



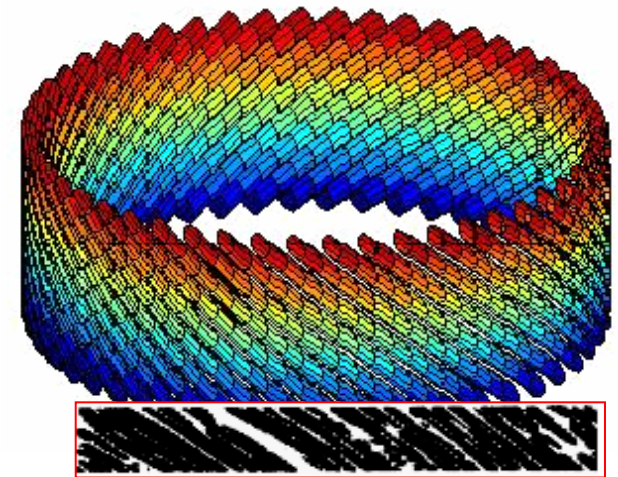
Whole left ventricle



endocardium

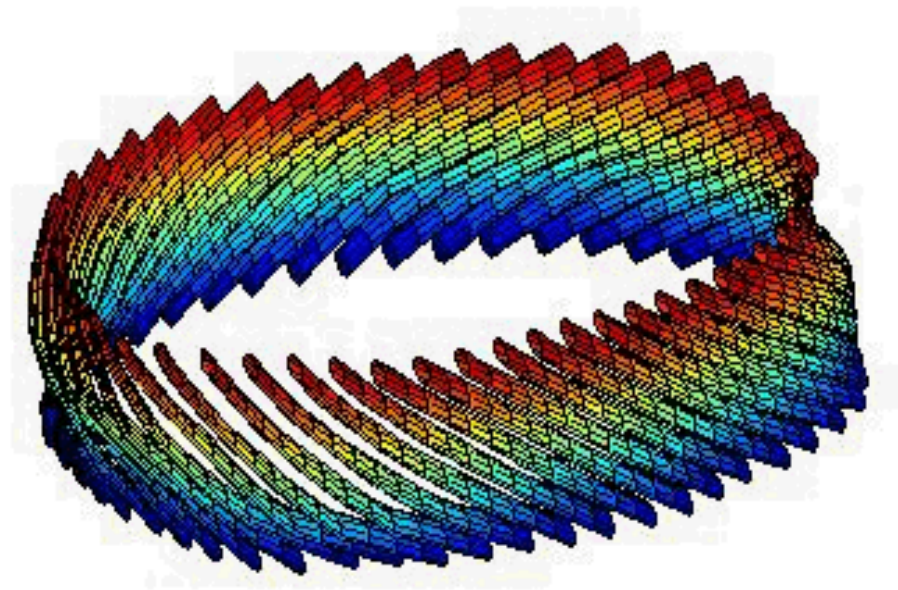
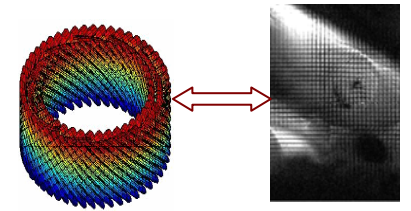


mid-wall



epicardium

3-D Reconstruction of the Epicardium



Conclusions

- Take into account the *myocardial fiber based structure*.
- Adopt the *continuum mechanics* framework.
- Implement *constrained energy minimization* algorithms.

